

A Suitable Power Transfer Control System for Interconnection Converter of DC Microgrids

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1. Brief Introduction

Local aggregation of Distributed Generation (DG) systems and electrical loads results in a Microgrid (μ G). In order to meet energy, reliability, power quality, power back-up and peak shaving needs and to allow sharing of resources within a common infrastructure, multiple μ Gs could be interconnected resulting in a power park [1]. Modern DG systems and modern electrical loads have DC link stages for interconnection to the AC distribution network. As a result, DC μ Gs provide the best solution for aggregation of these devices by integrating their DC power link stages. Previous researches have shown that DC μ Gs are preferable to both power frequency and high frequency AC μ Gs from various technical, economical and reliability viewpoints [2]-[7]. Thus, the DC Microgrid (DC μ G) concept and consequently, DC power parks have provided a new paradigm for future distribution power systems. The interconnection of DC μ Gs in a DC power park has not been studied in previous researches. In this paper, a DC/DC converter named Interconnection Converter (ICC) has been used for interconnection of two DC μ Gs. The main goal of this research is to develop a suitable control system for the DC/DC ICC.

Keywords

DC Microgrid, Distributed Generation, Droop Control, Hysteresis Current Control.

2. DC μ G Modeling

The typical structure of a DC μ G is shown in Fig. 1. All DC μ G converters are Voltage Source Converter (VSC) systems. The DC bus provides a common capacitive terminal for the VSCs.

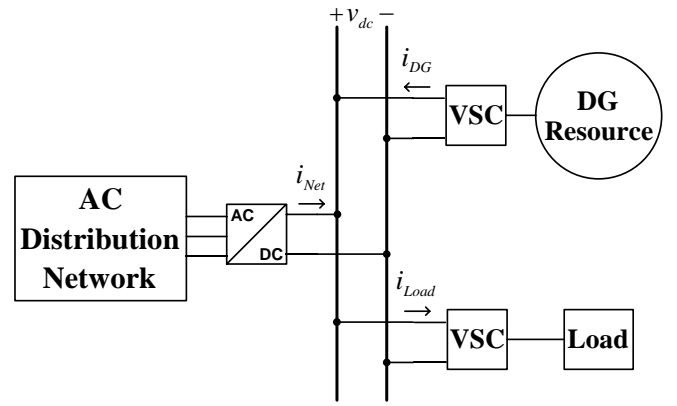


Fig. 1. Typical structure of DC μ G

The original and large signal values of the DC μ G bus voltage are the same, since the capacitive terminals of VSCs do not include high frequency switching waveforms [3]. As DC μ G bus voltages are the only signals from the DC μ Gs which interact with the DC/DC ICC, detailed and large signal modeling of the DC μ Gs would provide the same results for studying the DC/DC ICC. As a result, the large signal model of the DC μ G studied in [2] and [3] has been developed in this paper as illustrated in Fig. 2.

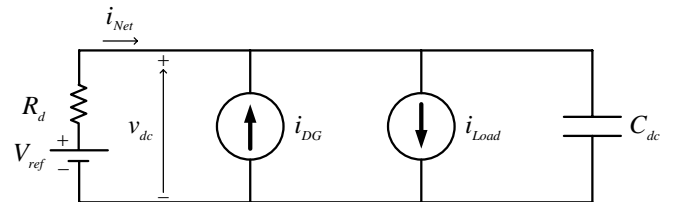


Fig. 2. DC μ G model

As shown in Fig. 2, the network converter is modeled as a DC voltage source in series with a droop resistor. The DG and load systems are modeled as independent current sources. The DC bus is modeled by the total required

capacitor for its VSCs. The design of the DC μ G parameters has been presented in details.

3. DC Power Park

Fig. 3 illustrates the DC power park which has been studied in this paper.

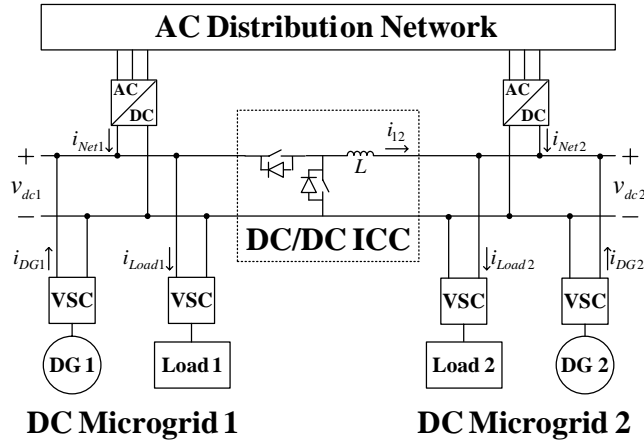


Fig. 3. DC power park

The DC/DC ICC has a DC/DC VSC topology with IGBT switches. The proposed control system for the DC/DC ICC should provide proper regulation of power flow and cancellation of interactions between the DC μ Gs. As a result, the DC/DC ICC control system should have fast dynamic response and insensitivity to system parameters variations. Hysteresis Current Control (HCC) is the simplest PWM system which has the above characteristics [9]. Thus, a two level HCC is used for the DC/DC ICC and its reference current is calculated as follows:

$$i_{12,ref} = \frac{P_{12,ref}}{v_{dc2}} \quad (1)$$

where $i_{12,ref}$ is the HCC reference current and $P_{12,ref}$ is the scheduled transfer power reference. As it can be seen, (1) is based on an instantaneous power regulation resulting in faster dynamic response than average power regulation methods. The maximum HCC switching frequency of the DC/DC ICC should be limited to an acceptable value. This issue has been considered in the design of the inductor L shown in Fig. 3.

4. Simulation Results

The system shown in Fig. 3 has been modeled and simulated by PSCAD/EMTDC. Large signal models of the DC μ Gs and detailed model of the DC/DC ICC has been used for modeling of the DC power park in this paper. As explained before, the large signal modeling of the DC μ Gs in this paper is just for simplification and it is not an approximation. In the first section, the system performance under changes of the scheduled transfer power reference is studied. In the second section, the

system performance under changes in active powers of the DG resource and the load in both DC μ Gs is studied. The steady state results have been verified by mathematical expressions. Simulation results indicate the good performance of the DC voltage droop controllers in adjusting the DC bus voltages within specified limits and the effectiveness of the proposed control system for the DC/DC ICC in the proper regulation of power transfer between the DC μ Gs. Furthermore, the DC bus voltage of either DC μ G is not changed due to changes in the DG or load power of the other DC μ G. As a result, disturbances in one DC μ G have no effect on the other DC μ G. This indicates the good performance of the proposed control system for the DC/DC ICC in cancellation of interactions between the DC μ Gs.

5. Conclusion

The operation and control strategies for the interconnection of DC μ Gs have not been studied in previous researches. In this paper, a suitable control strategy has been developed for a DC/DC voltage source converter which interconnects two DC μ Gs. A large signal model of DC μ Gs has also been developed which can effectively be used to study the interactions of DC μ Gs in a DC power park. Simulation results indicate that the proposed control strategy can properly regulate the instantaneous power transfer and can eliminate the interactions between interconnected DC μ Gs.

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